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European Technical Assessment Body for construction products



European Technical Assessment

ETA-25/0355 of 16 September 2025

English translation prepared by DIBt - Original version in German language

General Part

Technical Assessment Body issuing the European Technical Assessment:

Trade name of the construction product

Product family to which the construction product belongs

Manufacturer

Manufacturing plant

This European Technical Assessment contains

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of

Deutsches Institut für Bautechnik

Simpson Strong-Tie injection system EP-XP for rebar connection

System for post installed rebar connection with mortar

Simpson Strong-Tie Australia PTY Limited Unit 2A, 201 Power St NSW 2761 Glendenning AUSTRALIEN

Simpson Strong-Tie® Manufacturing Facilities

24 pages including 3 annexes which form an integral part of this assessment

EAD 330087-01-0601, Edition 06/2021

European Technical Assessment ETA-25/0355

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Specific Part

1 Technical description of the product

The subject of this European Technical Assessment is the post-installed connection, by anchoring or overlap connection joint, of reinforcing bars (rebars) in existing structures made of normal weight concrete, using the "Simpson Strong-Tie Injection system EP-XP for rebar connection" in accordance with the regulations for reinforced concrete construction.

Reinforcing bars made of steel with a diameter ϕ from 8 to 40 mm or the tension anchor ZA of sizes M12 to M24 according to Annex A and injection mortar EP-XP are used for rebar connections. The rebar is placed into a drilled hole filled with injection mortar and is anchored via the bond between rebar, injection mortar and concrete.

The product description is given in Annex A.

2 Specification of the intended use in accordance with the applicable European assessment Document

The performances given in Section 3 are only valid if the rebar connection is used in compliance with the specifications and conditions given in Annex B.

The verifications and assessment methods on which this European Technical Assessment is based lead to the assumption of a working life of the rebar connections of at least 50 and/or 100 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

3 Performance of the product and references to the methods used for its assessment

3.1 Mechanical resistance and stability (BWR 1)

Essential characteristic	Performance
Characteristic resistance under static and quasi-static loading	See Annex C 1
Characteristic resistance under seismic loading	See Annex B 4 and C 2

3.2 Safety in case of fire (BWR 2)

Essential characteristic	Performance
Reaction to fire	Class A1
Resistance to fire	See Annex C 3 to C 4

4 Assessment and verification of constancy of performance (AVCP) system applied, with reference to its legal base

In accordance with European Assessment Document EAD No. 330087-01-0601, the applicable European legal act is: [96/582/EC].

The system to be applied is: 1

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5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable European Assessment Document

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited with Deutsches Institut für Bautechnik.

Issued in Berlin on 16 September 2025 by Deutsches Institut für Bautechnik

Beatrix Wittstock beglaubigt:
Head of Section Baderschneider



Installation post installed rebar

Figure A1: Overlapping joint for rebar connections of slabs and beams

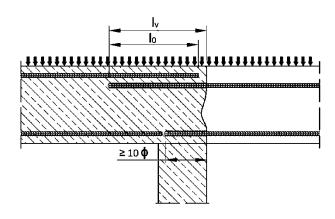


Figure A3: End anchoring of slabs or beams (e.g. designed as simply supported)

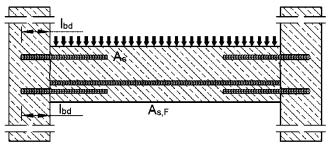


Figure A5: Anchoring of reinforcement to cover the line of acting tensile force

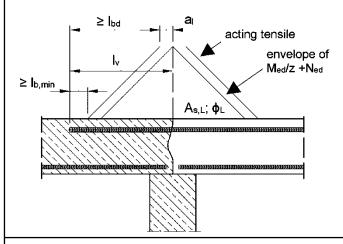


Figure A2: Overlapping joint at a foundation of a wall or column where the rebars are stressed in tension

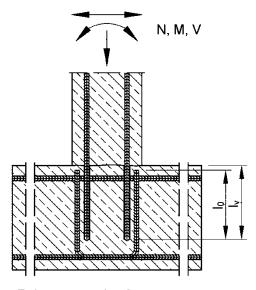
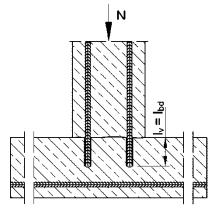


Figure A4: Rebar connection for components stressed primarily in compression. The rebars are stressed in compression



Note to Figure A1 to A5:

In the Figures no transverse reinforcement is plotted, the transverse reinforcement shall comply with EN 1992-1-1:2011.

Preparing of joints according to Annex B 2

Simpson Strong-Tie injection system EP-XP for rebar connection

Product description

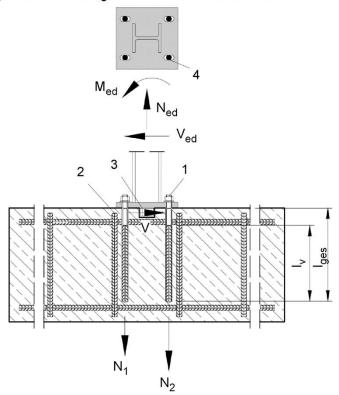
Installed condition and examples of use for rebars

Annex A 1



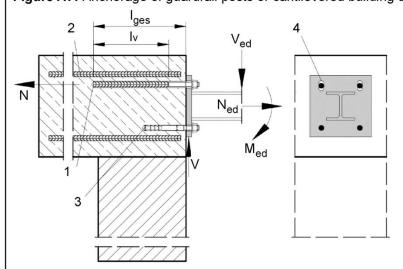
Installation tension anchor ZA

Figure A6: Anchorage of column to foundation with tension anchor ZA.



- 1 Tension anchor ZA (tension only)
- 2 Existing stirrup / reinforcement for overlap (lap splice)
- 3 Shear lug (or fastener loaded in shear)
- 4 Slotted hole with axial direction to the shear force

Figure A7: Anchorage of guardrail posts or cantilevered building components with tension anchor ZA and fastner.

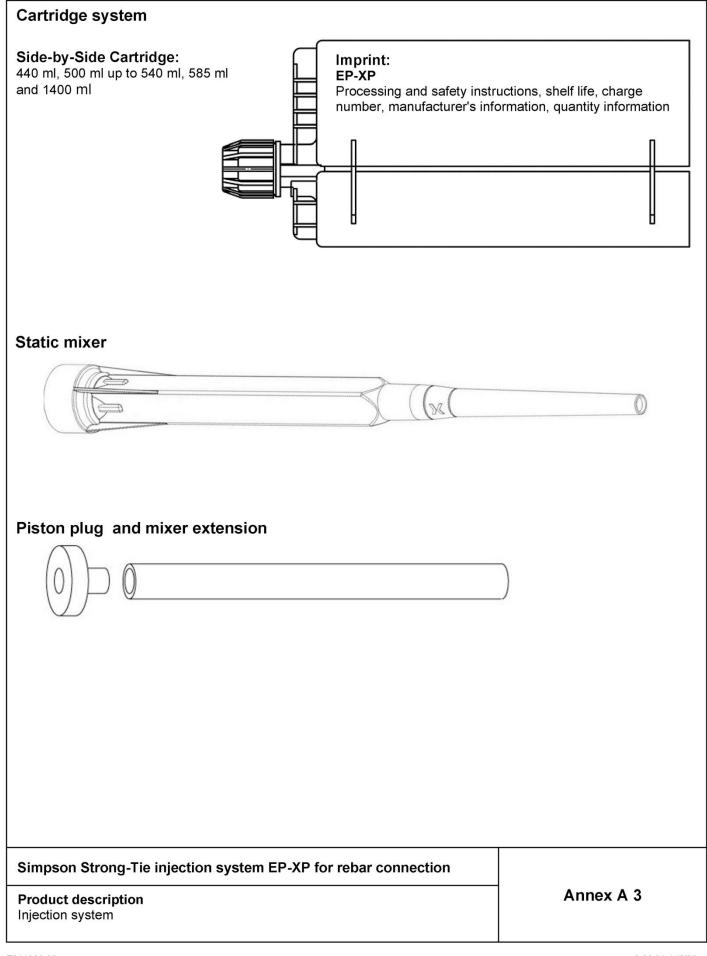


- 1 Tension anchor ZA (tension only)
- 2 Existing stirrup / reinforcement for overlap (lap splice)
- 3 Fastener (or shear lug loaded in shear)
- 4 Slotted hole with axial direction to the shear force

Note to Figure A6 and A7: In the Figures no transverse reinforcement is plotted, the transverse reinforcement shall comply with EN 1992-1-1:2011. The tension anchor may be only used for axial tensile force. The tensile force must be transferred by lab to the existing reinforcement of the building. The transfer of the shear force has to be ensured by suitable measures, e.g. by means of shear lugs or anchors with European Technical Assessment (ETA). Generals construction rules see Annex B 3

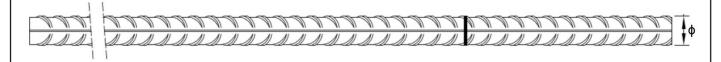
Simpson Strong-Tie injection system EP-XP for rebar connection Product description Installed condition and examples of use for tension anchors ZA Annex A 2







Reinforcing bar (rebar): ø8 up to ø40



- Minimum value of related rip area f_{R,min} according to EN 1992-1-1:2011
- Rib height of the bar shall be in the range 0,05φ ≤ h_{rib} ≤ 0,07φ
 (φ: Nominal diameter of the bar; h_{rib}: Rib height of the bar)

Table A1: Materials Rebar

Designation	Material
Rebar EN 1992-1-1:2011, Annex C	Bars and de-coiled rods class B or C f_{yk} and k according to NDP or NCL of EN 1992-1-1/NA f_{uk} = f_{tk} = $k \cdot f_{yk}$

Simpson Strong-Tie injection system EP-XP for rebar connection	
Product description Specifications Rebar	Annex A 4



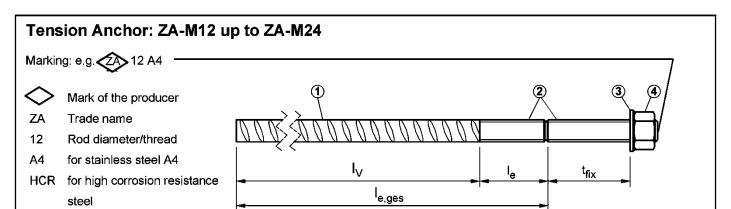


Table A2: Materials Tension Anchor ZA

		Material											
Part	Designation	ZA vz			ZA A4					ZA HCR			
		M12	M16	M20	M24	M12	M16	M20	M24	M12	M16	M20	M24
1	Reinforcement bar		Class B according to NDP or NCL of EN 1992-1-1/NA u _k = f _{tk} = k•f _{vk}						A				
	f _{yk} [N/mm²]	500				500			500				
2	Threaded rod	Steel, zinc plated according to EN ISO 683-4:2018 or EN 10263:2021				Stainless steel, 1.4362, 1.4401, 1.4404, 1.4571, EN 10088-1:2014			-	High corrosion resistant steel, 1.4529, 1.4565, EN 10088-1:2014			
3	Washer	Steel, zinc plated according			Stainless steel, 1.4362,			High corrosion resistant					
4	Nut	to EN ISO 683-4:2018 or EN 10263:2021			1.4401, 1.4404, 1.4571, EN 10088-1:2014		steel, 1.4529, 1.4565, EN 10088-1:2014						

Table A3: Dimensions and installation parameters

Size				ZA-M12	ZA-M16	ZA-M20	ZA-M24
Diameter of threa	aded rod	d _s	[mm]	12	16	20	24
Diameter of reinfo	orcement bar	ф	[mm]	12	16	20	25
Drill hole diamete	er	d _o	[mm]	14 or 16	20	25	30 or 32
Diameter of clear fixture	ance hole in	d _f	[mm]	14	18	22	26
With across nut f	lats	sw	[mm]	19	24	30	36
Stress area		A _s	[mm²]	84 157 245 353			
Effective embedr	nent depth	I _v	[mm]		according to st	atic calculation	
Length of	plated	1	[]	≥ 20	≥ 20	≥ 20	≥ 20
bonded thread	A4/HCR	⊣ 'e	[mm]	≥ 100	≥ 100	≥ 100	≥ 100
Minimum thickne	ss of fixture	min t _{fix}	[mm]	5	5	5	5
Maximum thickne	ess of fixture	max t _{fix}	[mm]	3000	3000	3000	3000
Maximum installa	ation torque	max T _{inst}	[Nm]	50	100	150	150

Simpson Strong-Tie injection system EP-XP for rebar connection	
Product description Specifications Tension Anchor ZA	Annex A 5



Specification of the intended use					
Anchorages subject to:		Working life 50 years	Working life 100 years		
HD: Hammer drilling	static and quasi-static loads	Ø8 to Ø40 ZA-M12 to ZA-M24	Ø8 to Ø40 ZA-M12 to ZA-M24		
HDB: Hammer drilling with hollow drill bit	seismic action	Ø10 to Ø40	Ø10 to Ø40		
CD: Compressed air drilling DD: Diamond drilling	fire exposure	Ø8 to Ø40 ZA-M12 to ZA-M24	Ø8 to Ø40 ZA-M12 to ZA-M24		
Temperature Range: - 40°C to +80°C (max long-term temperature +50 °C and max short-term temperature +80 °C)					

Base materials:

- Reinforced or unreinforced normal weight concrete according to EN 206:2013 + A1:2016.
- Strength classes C12/15 to C50/60 according to EN 206:2013 + A1:2016.
- Maximum chloride content of 0,40% (CL 0.40) related to the cement content according to EN 206:2013 + A1:2016.
- Non-carbonated concrete.

Note: In case of a carbonated surface of the existing concrete structure the carbonated layer shall be removed in the area of the post-installed rebar connection with a diameter of $\phi + 60$ mm prior to the installation of the new rebar.

The depth of concrete to be removed shall correspond to at least the minimum concrete cover in accordance with EN 1992-1-1:2011. The foregoing may be neglected if building components are new and not carbonated and if building components are in dry conditions.

Use conditions (Environmental conditions) with tension anchor ZA:

- Structures subject to dry internal conditions (all materials).
- For all other conditions according to EN 1993-1-4:2006 + A1:2015 corresponding to corrosion resistance class:
 - Stainless steel class A4 according to Annex A 5, Table A2: CRC III
 - High corrosion resistance steel HCR according to Annex A 5, Table A2: CRC V

Design:

- Anchorages are designed under the responsibility of an engineer experienced in anchorages and concrete work.
- Verifiable calculation notes and drawings are prepared taking account of the forces to be transmitted.
- Design according to EN 1992-1-1:2011, EN 1992-1-2:2011 and Annex B 2 and B 3.
- The actual position of the reinforcement in the existing structure shall be determined on the basis of the construction documentation and taken into account when designing.

Installation:

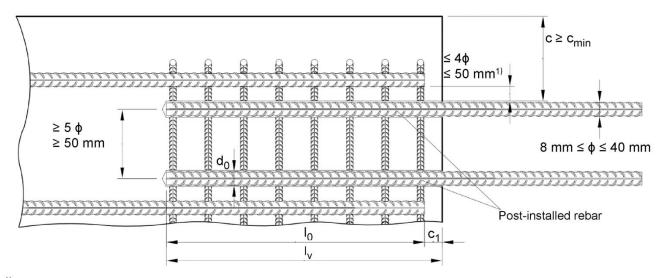
- Dry or wet concrete. It must not be installed in flooded holes.
- Overhead installation allowed.
- Hole drilling by hammer drill (HD), hollow drill (HDB), diamond drill (DD) or compressed air drill mode (CD).
- The installation of post-installed rebar resp. tension anchors shall be done only by suitable trained installer and under supervision on site; the conditions under which an installer may be considered as suitable trained and the conditions for supervision on site are up to the Member States in which the installation is done.
- Check the position of the existing rebars (if the position of existing rebars is not known, it shall be determined using a rebar detector suitable for this purpose as well as on the basis of the construction documentation and then marked on the building component for the overlap joint).

Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use Specifications	Annex B 1



Figure B1: General construction rules for post-installed rebars

- Only tension forces in the axis of the rebar may be transmitted.
- The transfer of shear forces between new concrete and existing structure shall be designed additionally according to EN 1992-1-1:2011.
- The joints for concreting must be roughened to at least such an extent that aggregate protrude.



1) If the clear distance between lapped bars exceeds 4φ or 50 mm, then the lap length shall be increased by the difference between the clear bar distance and the smaller of 4φ or 50 mm.

The following applies to Figure B1:

c concrete cover of post-installed rebar

concrete cover at end-face of existing rebar

c_{min} minimum concrete cover according to Table B1 and to EN 1992-1-1:2011, Section 4.4.1.2

φ diameter of post-installed rebar

 ${\rm I}_{\rm 0}$ Lap length, according to EN 1992-1-1:2011, section 8.7.3 for static loading and according to

EN 1998- 1:2004+AC:2009, section 5.6.3 for seismic action

 I_v effective embedment depth, $\geq I_0 + c_1$

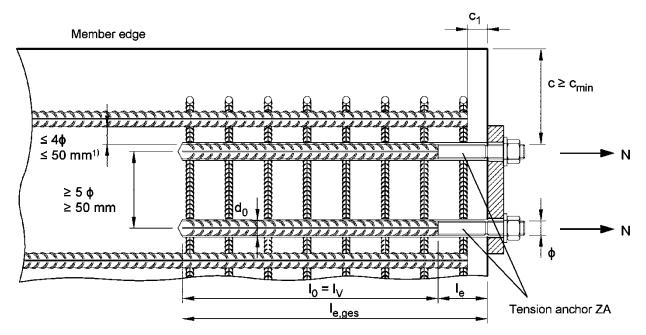
 ${\rm d_0}$ nominal drill bit diameter, see Annex B 5

Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use General construction rules for post-installed rebars	Annex B 2



Figure B2: General construction rules for tension anchors ZA

- The length of the bonded-in thread may be not be accounted as anchorage.
- Only tension forces in the direction of the bar axis may be transmitted by the tension anchor ZA.
- The tension force must be transferred via an overlap joint to the reinforcement in the building part.
- The transfer of shear forces shall be ensured by appropriate additional measures, e.g shear lugs or by anchors with an European technical assessment.
- In the anchor plate, the holes for the tension anchors shall be executed as elongated holes with axis in the direction of the shear force.



1) If the clear distance between lapped bars exceeds 4φ or 50 mm, then the lap length shall be increased by the difference between the clear bar distance and the smaller of 4φ or 50 mm.

The following applies to Figure B2:

c concrete cover of tension anchor ZA

c₁ concrete cover at end-face of existing rebar

c_{min} minimum concrete cover according to Table B1 and to EN 1992-1-1:2011, Section 4.4.1.2

φ diameter of tension anchor

l₀ lap length, according to EN 1992-1-1:2011, Section 8.7.3

I_v effective embedment depthI_e length of bonded thread

 $I_{e,ges}$ overall embedment depth, $\ge I_0 + c_2$

d₀ nominal drill bit diameter, see Annex B 5

Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use General construction rules for tension anchors ZA	Annex B 3



Table B1:	Minimum concrete cover c _{min} 1) of post-installed rebar and tie rod ZA
	depending of drilling method

WORLD A CONTROL OF THE SECOND STATE OF THE SEC								
Drilling method	Rebar diameter	Without drilling aid	With dri	lling aid				
HD: Hammer drilling HDB: Hammer drilling	< 25 mm	30 mm + 0,06 · I _v ≥ 2 ф	30 mm + 0,02 · I _V ≥ 2 φ					
with hollow drill bit	≥ 25 mm	40 mm + 0,06 · l _v ≥ 2 φ	40 mm + 0,02 · l _v ≥ 2 φ	Drilling aid				
DD: Diamond drilling	< 25 mm	Drill rig used as drilling	30 mm + 0,02 · l _v ≥ 2 φ					
DD. Diamond dilling	≥ 25 mm	aid	40 mm + 0,02 · l _v ≥ 2 φ					
CD: Compressed air	< 25 mm	50 mm + 0,08 · l _v	50 mm + 0,02 · l _v	д				
drilling	≥ 25 mm	60 mm + 0,08 · l _v ≥ 2 ф	60 mm + 0,02 · I _v ≥ 2 φ					

¹⁾ see Annex B 2, Figure B1 and Annex B 3, Figure B2
Comments: The minimum concrete cover acc. EN 1992-1-1:2011 must be observed.

For the minimum concrete cover cmin, seis in case of a seismic action, see Table B2.

Table B2: Minimum concrete cover min $c_{\text{min,seis}}$

Drilling method	Design conditions	Distance to 1st edge	Distance to 2nd edge
HD: Hammer drilling HDB: Hammer drilling with	Edge	≥ 2 ф	≥ 2 ф
hollow drill bit CD: Compressed air drilling	Corner	≥ 2 ф	≥ 2 ф
DD: Diamond drilling	Edge	≥ 4 ф	≥ 8 ф
Diamond drilling	Corner	≥ 6 ф	≥ 6 ф

Table B3: Dispensing tools

Cartridge type/size	На	nd tool	Pneumatic tool
Side-by-side cartridges 440 ml, 500 ml up to 540 ml, 585 ml			
	e.g. SA 296C585	e.g. Type H 244 C	e.g. Type TS 444 KX
Side-by-side cartridges 1400 ml	-	-	e.g. Type TS 471

All cartridges could also be extruded by a battery tool.

Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use Minimum concrete cover Dispensing tools	Annex B 4



Table B4:	Brushes, piston plugs, max anchorage depth and mixer extension, hammer
	(HD), diamond (DD) and compressed air (CD) drilling

						<u> </u>										
_			Drill				d _{b,min}		Cartr	idge: 440, 50	0-540	or 585 ml	Cartri	dge: 1400 ml		
Bar size	Tension anchor	l	bit - Ø		d _b		d _b Brush - Ø		min. Brush -	min. Piston		Hand or battery tool		matic tool	Pneumatic tool	
ф	ф	HD	DD	CD	Dius		Ø	piag	I _{v,max}	Mixer extension	I _{v,max}	Mixer extension	I _{v,max}	Mixer extension		
[mm]	[mm]		[mm]			[mm]	[mm]		[mm]		[mm]		[mm]			
8	_	1	0	_	RB10	11,5	10,5	-	250		250		250			
	-	'	0	_	RB12	13,5	12,5	_	700		800		800	10/0,75		
10	-	1	2		IND 12	13,3	12,3	_	250		250		250	or		
	-	'		_	RB14	15,5	14,5	14	700		1000		1000	16/1,8		
12	ZA-M12	1	4	-	KB 14	13,3	14,5	14	250		250		250			
12	ZA-101 1Z		16		RB16	17,5	16,5	16					1200			
14	-		18		RB18	20,0	18,5	18	700	40/0 75	1300		1400			
16	ZA-M16		20		RB20	22,0	20,5	20		10/0,75 or 16/1,8			1600			
20	ZA-M20	2	5	-	RB25	27,0	25,5	25		10/1,0		10/0,75 or				
	ZA-10120	,	-	26	RB26	28,0	26,5	25				16/1,8				
22	-		28		RB28	30,0	28,5	28								
24/25	7A M24		30		RB30	32,0	30,5	30	500					16/1,8		
24/25	ZA-M24		32		RB32	34,0	32,5	32			4000		2000			
28	-		35		RB35	37,0	35,5	35			1000		2000			
32/34	-		40		RB40	43,5	40,5	40								
36	-		45		RB45	47,0	45,5	45								
40	_	-	52	52	RB52	54,0	52,5	52	-	-						
40	_	55	-	55	RB55	58,0	55,5	55								

Table B5: Brushes, piston plugs, max anchorage depth and mixer extension, hammer drilling with hollow drill bit system (HDB)

	_	Drill		d _{b,min}		Cart	ridge: 440, 5	00-540 d	or 585 ml	Cartrid	ge: 1400 ml
Bar size	Tension anchor	bit - Ø	d _b	min.	Piston plug	Hand or	battery tool	Pneu	matic tool	Pneu	matic tool
φ	φ	HDB	Brush - Ø	Ø	piug	I _{v,max}	Mixer extension	$I_{v,max}$	Mixer extension	$I_{v,max}$	Mixer extension
[mm]	[mm]	[mm]				[mm]		[mm]		[mm]	
8	-	10			-	250		250		250	
	-	12				700		800		800	
10	_	12			-	250		250		250	
10	-	4.4			14	700		1000	1000 250	1000	
40	70 8440	14				250		250		250	
12	ZA-M12	16		No cleaning 18 18	16	700					
14	-	18					10/0,75 or		10/0,75 or		10/0,75 or
16	ZA-M16	20	requi	rea	20]	16/1,8		16/1,8		16/1,8
20	ZA-M20	25			25						
22		28			28]		1000		1000	
04/05	74 1404	30			30	500					
24/25	ZA-M24	32			32	500					
28		35			35						
32/34		40			40						

Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use	Annex B

Parameter brushes, piston plugs, max anchorage depth and mixer extension

Z211036.25 8.06.01-117/25

5



Cleaning and installation tools

HDB - Hollow drill bit system



The hollow drill system consists of Heller Duster Expert or a hollow drill bit with equivalent performance and a class M vacuum cleaner with a minimum negative pressure of 253 hPa and a flow rate of minimum 150 m³/h (42 l/s).

Hand pump

(Volume 750 ml, $h_0 \le 10 d_s$, $d_0 \le 20 mm$)



Manual slide valve

(min 6 bar)



Brush RB



Piston Plug



Brush extension RBL



Table B6: Working time and curing time

Tempera	ature in bas	e material	Maximum working time	Initial curing time ¹⁾	Minimum curing time ²⁾
	Т		t _{work}	t _{cure,ini}	t _{cure}
0°C	up to	+ 4 °C	80 min	30 h	144 h
+ 5°C	up to	+ 9°C	80 min	20 h	48 h
+ 10°C	up to	+ 14 °C	60 min	15 h	28 h
+ 15°C	up to	+ 19°C	40 min	9 h	18 h
+ 20 °C	up to	+ 24 °C	30 min	6 h	12 h
+ 25 °C	up to	+ 34 °C	12 min	4 h	9 h
+ 35°C	up to	+ 39 °C	8 min	3 h	6 h
	+40°C		8 min	1,5 h	4 h
Car	tridge tempe	rature		+5°C up to +40°C	

¹⁾ After Initial curing time has elapsed, the installation of the connecting reinforcement and the construction of the formwork can be continued

²⁾ The minimum curing time is only valid for dry base material. In wet base material the curing time must be doubled.

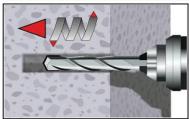
Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use Cleaning and installation tools Working time and curing time	Annex B 6



Installation instructions

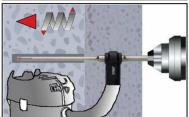
Attention: Before drilling, remove carbonated concrete and clean contact areas (see Annex B1) In case of aborted drill hole: the drill hole shall be filled with mortar.

Drilling of the bore hole



Hammer drilling (HD) / Compressed air drilling (CD) Drill a hole to the required embedment depth.

Drill bit diameter according to Table B4.
Proceed with Step 2 (MAC or CAC).



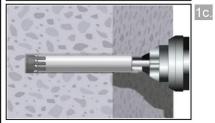
Hollow drill bit system (HDB) (see Annex B 6)

Drill a hole to the required embedment depth.

Drill bit diameter according to Table B5.

The hollow drilling system removes the dust and closes to

The hollow drilling system removes the dust and cleans the bore hole. Proceed with Step 3.



Diamond drilling (DD)

Drill a hole to the required embedment depth Drill bit diameter according to Table B4. Proceed with Step 2 (SPCAC).

Simpson Strong-Tie injection system EP-XP for rebar connection

Intended use
Installation instruction

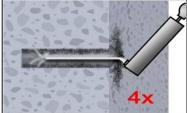
Annex B 7



Installation instructions (continuation)

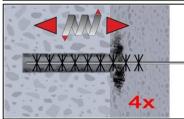
Manual Air Cleaning (MAC)

for drill hole diameter $d_0 \le 20$ mm and drill hole depth $h_0 \le 10$ with drilling method HD/CD

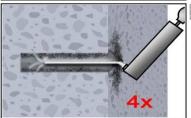


Attention! Standing water in the bore hole must be removed before cleaning.

Blow the bore hole clean minimum 4x from the bottom or back by hand pump (Annex B 6).



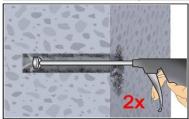
Brush the bore hole minimum 4x with brush RB according to Table B4 over the entire embedment depth in a twisting motion (if necessary, use a brush extension RBL).



Finally blow the bore hole clean minimum 4x from the bottom or back by hand pump (Annex B 6).

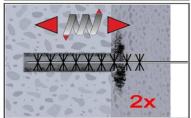
Compressed Air Cleaning (CAC):

All diameter with drilling method HD/CD

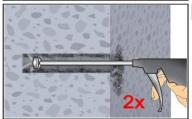


Attention! Standing water in the bore hole must be removed before cleaning.

2a. Blow the bore hole clean minimum 2x with compressed air (min. 6 bar, oil-free) (Annex B 6) over the entire embedment depth until return air stream is free of noticeable dust. (If necessary, an extension shall be used.)



Brush the bore hole minimum 2x with brush RB according to Table B4 over the entire embedment depth in a twisting motion. (If necessary, a brush extension shall be used.)



Finally blow the bore hole clean minimum 2x with compressed air (min. 6 bar, oil-free) (Annex B 6) over the entire embedment depth until return air stream is free of noticeable dust. (If necessary, an extension shall be used.)

Protect cleaned bore hole against re-contamination in an appropriate way. If necessary, repeat cleaning process directly before dispensing the mortar. In-flowing water must not contaminate the bore hole again.

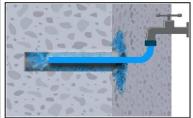
Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use Installation instructions (continuation)	Annex B 8



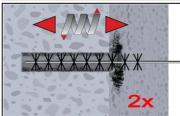
Installation instructions (continuation)

Flush & Compressed Air Cleaning (SPCAC):

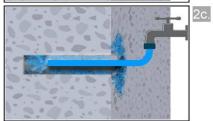
All diameter with drilling method DD



2a. Flushing with water until clear water comes out.

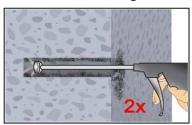


2b. Brush the bore hole minimum 2x with brush RB according to Table B4 over the entire embedment depth in a twisting motion. (If necessary, a brush extension shall be used.)

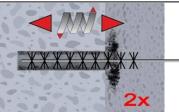


Flushing again with water until clear water comes out.

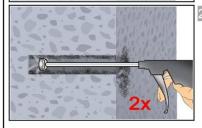
Attention! Standing water in the bore hole must be removed before proceeding.



Blow the bore hole clean minimum 2x with compressed air (min. 6 bar, oil-free) (Annex B 6) over the entire embedment depth until return air stream is free of noticeable dust. (If necessary, an extension shall be used.)



Brush the bore hole minimum 2x with brush RB according to Table B4 over the entire embedment depth in a twisting motion. (If necessary, a brush extension shall be used.)

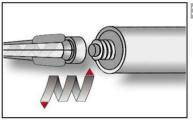


Finally blow the bore hole clean minimum 2x with compressed air (min. 6 bar, oil-free) (Annex B 6) over the entire embedment depth until return air stream is free of noticeable dust. (If necessary, an extension shall be used.)

Protect cleaned bore hole against re-contamination in an appropriate way. If necessary, repeat cleaning process directly before dispensing the mortar. In-flowing water must not contaminate the bore hole again.

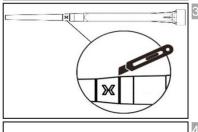
Simpson Strong-Tie injection system EP-XP for rebar connection	
Intended use Installation instructions (continuation)	Annex B 9

Installation instructions (continuation)

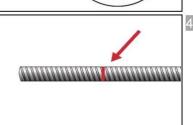


Screw on static-mixing nozzle MNXP, and load the cartridge into an appropriate dispensing tool.

For every working interruption longer than the maximum working time t_{work} (Annex B 6) as well as for new cartridges, a new static-mixer shall be used.



In case of using the mixer extension 16/1,8, cut off the tip of the mixer nozzle at position "X".



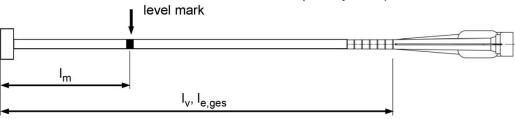
Mark embedment depth on the reinforcing bar .

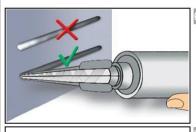
The reinforcing bar shall be free of dirt, grease, oil or other foreign material.

Mark mixer nozzle and extension with mortar level mark Im and anchorage depth Iv resp. $I_{e,ges}$ Quick estimation: $I_{e,ges}$

Quick estimation: $I_m = 1/3 \cdot I_v$ Optimum mortar volume:

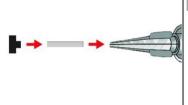
$$I_{m} = I_{v} \text{ resp. } I_{e,ges} \cdot \left(1,2 \cdot \frac{\phi^{2}}{d_{0}^{2}} - 0,2\right)$$





Not proper mixed mortar is not sufficient for fastening.

Dispense and discard mortar until an uniform grey or red colour is shown (at least 3 full strokes).



Piston plugs and mixer nozzle extensions shall be used according to Table B4 or B5.

Assemble mixing nozzle, mixer extension and piston plug before injecting mortar.

Simpson Strong-Tie injection system EP-XP for rebar connection

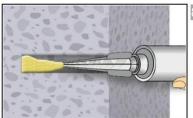
Intended use

Installation instructions (continuation)

Annex B 10

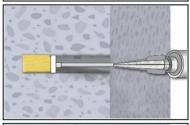


Installation instructions (continuation)



8a. Injecting mortar without piston plug:

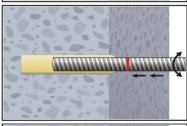
Starting at bottom of the hole and fill the hole with adhesive until the mortar level mark is visible. (If necessary, a mixer nozzle extension shall be used.) Slowly withdraw of the static mixing nozzle avoid creating air pockets Observe the temperature related working time t_{work} (Annex B 6).



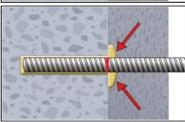
Injecting mortar with piston plug:

Insert piston plug to bottom of the hole and fill the hole with mortar until mortar level mark l_m is visible. (If necessary, a mixer nozzle extension shall be used.) During injection the piston plug is pushed out of the bore hole by the back pressure of the mortar.

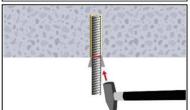
Observe the temperature related working time t_{work} (Annex B 6).



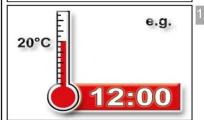
Insert the reinforcing bar while turning slightly up to the embedment mark.



Annular gap between reinforcing bar and base material must be completely filled with mortar. Otherwise, the installation must be repeated starting from step 8 before the maximum working time t_{work} has expired.



For application in vertical upwards direction the reinforcing bar shall be fixed (e.g. wedges).



Temperature related curing time t_{cure} (Annex B 6) must be observed. After initial curing time $t_{cure,ini}$ has elapsed, the installation of the connecting reinforcement and the formwork can be continued. The full load to the reinforcing bar may be applied after the full curing time t_{cure} has elapsed.

Simpson Strong-Tie injection system EP-XP for rebar connection
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Intended use

Installation instructions (continuation)

Annex B 11



Table C1: Characteristic tension resistance for tension anchor ZA									
Tension Anchor ZA-M12 ZA-M16 ZA-M20 ZA-M24									
Steel, zinc plated (ZA vz)									
Characteristic tension resistance	$N_{Rk,s}$	[kN]	67	125	196	282			
Partial factor	γMs,N	[-]		1	,4				
Stainless Steel (ZA A4 or ZA HCR	()								
Characteristic tension resistance	$N_{Rk,s}$	[kN]	67 125 171 247						
Partial factor	γ _{Ms,N}	[-]	1,4 1,3 1,4						

Minimum anchorage length and minimum lap length under static or quasi-static loading

The minimum anchorage length $I_{b,min}$ and the minimum lap length $I_{0,min}$ according to EN 1992-1-1:2011 ($I_{b,min}$ acc. to Eq. 8.6 and Eq. 8.7 and $I_{0,min}$ acc. to Eq. 8.11) shall be multiply by the amplification factor $\alpha_{lb} = \alpha_{lb,100y}$ according to Table C2.

Table C2: Amplification factor $\alpha_{lb} = \alpha_{lb,100y}$ related to concrete class and drilling method; working life 50 and 100 years

Concrete class	Drilling method	Bar size	Amplification factor $\alpha_{lb} = \alpha_{lb,100y}$
C12/15 to C50/60	all drilling methods	8 mm to 40 mm ZA-M12 to ZA-M24	1,0

Table C3: Reduction factor $k_b = k_{b,100y}$ for all drilling methods; working life 50 and 100 years

Rebar				Co	ncrete cla	ass			
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
8 to 40 mm ZA-M12 to ZA-M24					1,0				

Table C4: Design values of the ultimate bond stress $f_{bd,PIR}$ and $f_{bd,PIR,100y}$ in N/mm² for all drilling methods and for good conditions; working life 50 and 100 years

 $f_{bd,PIR} = k_b \cdot f_{bd}$ $f_{bd,PIR,100y} = k_{b,100y} \cdot f_{bd}$

with

 f_{bd} : Design value of the ultimate bond stress in N/mm² considering the concrete classes, the rebar diameter, the drilling method for good bond condition (for all other bond conditions multiply the values by η_1 =0.7) and recommended partial factor γ_c = 1,5 according to EN 1992-1-1:2011.

k_b, k_{b.100v}: Reduction factor according to Table C3

Rebar		Concrete class							
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
8 to 32 mm ZA-M12 to ZA-M24	1,6	2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3
34 mm	1,6	2,0	2,3	2,6	2,9	3,3	3,6	3,9	4,2
36 mm	1,5	1,9	2,2	2,6	2,9	3,3	3,6	3,8	4,1
40 mm	1,5	1,8	2,1	2,5	2,8	3,1	3,4	3,7	4,0

Simpson Strong-Tie injection system EP-XP for rebar connection

Performances

Characteristic tension resistance for tension anchor, Minimum anchorage length and minimum lap length, Amplification factor, Reduction factor and Design values of ultimate bond resistance

Annex C 1



Minimum anchorage length and minimum lap length under seismic action

The minimum anchorage length $I_{b,min}$ and the minimum lap length $I_{0,min}$ according to EN 1992-1-1:2011 ($I_{b,min}$ acc. to Eq. 8.6 and Eq. 8.7 and $I_{0,min}$ acc. to Eq. 8.11) shall be multiply by the amplification factor $\alpha_{lb,seis,100y}$ according to Table C5.

Table C5: Amplification factor $\alpha_{lb,seis} = \alpha_{lb,seis,100y}$ related to concrete class and drilling method; working life 50 and 100 years

Concrete class	Drilling method	Bar size	Amplification factor $\alpha_{\text{lb,seis}} = \alpha_{\text{lb,seis,100y}}$
C16/20 to C50/60	all drilling methods	10 mm to 40 mm	1,0

Table C6: Reduction factor $k_{b,seis} = k_{b,seis,100y}$ for all drilling methods; working life 50 and 100 years

Rebar				Concre	te classe	s			
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
10 to 40 mm	No performance assessed				1	,0			

Table C7: Design values of the ultimate bond stress $f_{bd,PIR,seis}$ and $f_{bd,PIR,seis,100y}$ in N/mm² for all drilling methods and for good conditions; working life 50 and 100 years

 $f_{bd,PIR,seis} = k_{b,seis+fbd}$

 $f_{bd,PIR,seis,100y} = k_{b,seis,100y \cdot fbd}$

with

 f_{bd} : Design value of the ultimate bond stress in N/mm² considering the concrete classes, the rebar diameter, the drilling method for good bond condition (for all other bond conditions multiply the values by η_1 =0.7) and recommended partial factor γ_c = 1,5 according to EN 1992-1-1:2011.

 $k_{b,seis}, k_{b,seis,100v}$: Reduction factor according to Table C6

Rebar	Concrete classes								
ф	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
10 to 32 mm		2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3
34 mm	No performance	2,0	2,3	2,6	2,9	3,3	3,6	3,9	4,2
36 mm	assessed	1,9	2,2	2,6	2,9	3,3	3,6	3,8	4,1
40 mm		1,8	2,1	2,5	2,8	3,1	3,4	3,7	4,0

Simpson Strong-Tie injection system EP-XP for rebar connection	
Performances Minimum anchorage length and minimum lap length, Amplification factor, Reduction factor and Design values of ultimate bond stress under seismic action	Annex C 2



Design value of the ultimate bond stress $f_{bd,fi}$, $f_{bd,fi,100y}$ at increased temperature for concrete classes C12/15 to C50/60, (all drilling methods); working life 50 and 100 years:

The design value of the bond stress f_{bd fi} at increased temperature has to be calculated by the following equation:

For working life 50 years: $f_{bd,fi} = k_{fi}(\theta) \cdot f_{bd,PIR} \cdot \gamma_c / \gamma_{M,fi}$

 $k_{fi}(\theta) = 4673.8 \cdot \theta^{-1.598} / (f_{bd,PIR} \cdot 4.3) \le 1.0$ θ ≤ 278°C: with:

> $k_{fi}(\theta) = 0$ $\theta > 278^{\circ}C^{\circ}$

For working life 100 years:

$$\begin{split} f_{bd,fi,100y} &= k_{fi,100y}(\theta) \, \cdot \, f_{bd,PIR,100y} \, \cdot \, \gamma_c \, / \, \gamma_{M,fi} \\ k_{fi,100y}(\theta) &= \, \, 4673,8 \, \cdot \, \theta^{-1,598} \, / \, \, (f_{bd,PIR,100y} \cdot \, 4,3) \leq 1,0 \end{split}$$
θ ≤ 278°C:

 $\theta > 278^{\circ}C$: $k_{fi,100v}(\theta) = 0$

Design value of the ultimate bond stress at increased temperature in N/mm² f_{bd,fi, fbd,fi,100y}

Temperature in °C in the mortar layer.

 $k_{fi}(\theta), k_{fi,100v}(\theta)$ Reduction factor at increased temperature.

Design value of the bond stress $f_{bd,PIR} = f_{bd,PIR,100y}$ in N/mm² in cold condition according to f_{bd,PIR}, f_{bd,PIR,100y}

Table C4 considering the concrete classes, the rebar diameter, the drilling method and the bond

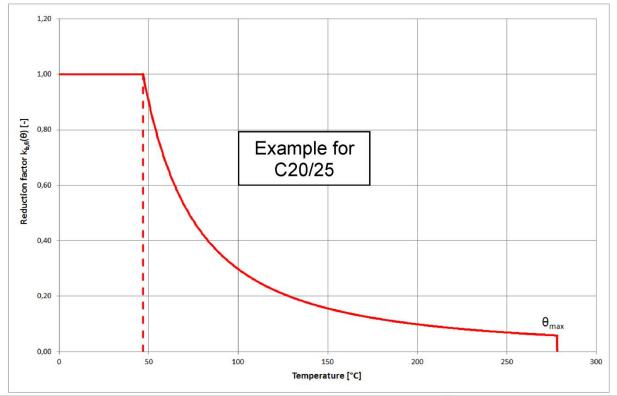
conditions according to EN 1992-1-1:2011.

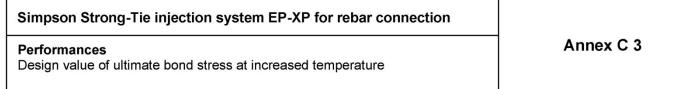
= 1,5, recommended partial factor according to EN 1992-1-1:2011 γ_{c}

= 1,0, recommended partial factor according to EN 1992-1-2:2011

For evidence at increased temperature the anchorage length shall be calculated according to EN 1992-1-1:2011 Equation 8.3 using the temperature-dependent design value of ultimate bond stress $f_{bd,fi}$, $f_{bd,fi,100y}$.

Example graph of Reduction factor $k_{fi}(\theta)$, $k_{fi.100v}(\theta)$ for concrete classes C20/25 for good bond conditions:







Tension Anchor	•			ZA-M12	ZA-M16	ZA-M20	ZA-M24
Steel, zinc plated	(ZA vz)						
Characteristic	R30			2,3	4,0	6,3	9,0
	R60	NI NI	[kN]	1,7	3,0	4,7	6,8
tension resistance	R90	$N_{Rk,s,fi}$		1,5	2,6	4,1	5,9
	R120			1,1	2,0	3,1	4,5
Stainless Steel (2	ZA A4 or Z	A HCR)					
	R30			3,4	6,0	9,4	13,6
Characteristic	R60	N.	£1 b 13	2,8	5,0	7,9	11,3
-	R90	$N_{Rk,s,fi}$	[kN]	2,3	4,0	6,3	9,0
	R120			1,8	3,2	5,0	7,2

Simpson Strong-Tie injection system EP-XP for rebar connection	
Performances Characteristic tension resistance for tension anchor ZA under fire exposure	Annex C 4